## INSTALLATION PARAMETERS AND APPLIED FORCES TO THE SUPPORTING STRUCTURE

The applied forces drawing in diagram 1, details the relative position and the direction of forces that the work station bridge crane applies to the supporting structure.

Loads applied to the support structure can be determined by the following formulas:
$P=$ Live Load
R1 = Vertical Load applied by support hanger (lb.)
R2 $=$ Longitudinal load applied by movement of the crane to each runway (lb.)
R3 $=$ Lateral load applied by movement of the trolley and load to each runway (lb.)
$\mathrm{L} 1=$ Maximum distance between hanger centerlines (support centers) (ft)
L2 $=$ Maximum splice joint centerline to hanger centerline (support center) (in)

Diagram 1. Applied forces to supporting structure.
L5 $=$ Maximum bridge cantilever (in)
L9 $=$ Maximum runway cantilever (in)
L4 $=$ Bridge span (distance between runway centerlines) ( ft )
$1.4=$ Design factor which includes 25\% for impact and $15 \%$ for hoist weight
$W$ = Weight per foot of runway (lb./ft)
$w=$ Weight per foot of bridge ( $\mathrm{lb} . / \mathrm{ft}$ )

Note: If there are only 2 hangers per runway substitute "(L1)/2" for "L1" in the R1 formula.

Note: For bridge lengths greater than 23 ft ., up to 28 ft ., use GLCSL weights. Greater than 28 ft . lengths, up to 34 ft ., use GLCSLX weights.

| INSTALLATION PARAMETERS |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CAPACITY | SERIES | WEIGHT PER FOOT | $\begin{gathered} \text { MAX. } \\ \hline \end{gathered}$ | $\begin{gathered} \text { MAX. } \\ \text { L2 } \\ \hline \end{gathered}$ | $\begin{gathered} \text { MAX. } \\ \hline \end{gathered}$ | $\begin{gathered} \text { MAX. } \\ \hline \\ \hline \end{gathered}$ |
| 250\# | GLC | 2.53\# | 6 | $8{ }^{\prime \prime}$ | $18^{\prime \prime}$ | $18^{\prime \prime}$ |
|  | GLCS | 4.92\# | $20^{\prime}$ | $48^{\prime \prime}$ | 18 " | $48^{\prime \prime}$ |
|  | AL | 4.05\# | $20^{\prime}$ | $30^{\prime \prime}$ | $48^{\prime \prime}$ | $48^{\prime \prime}$ |
|  | GLCSL | 8.43\# | $25^{\prime}$ | $48^{\prime \prime}$ | $18^{\prime \prime}$ | $48^{\prime \prime}$ |
| 500\# | GLC | 4.11\# | 6 | $8{ }^{\prime \prime}$ | $24^{\prime \prime}$ | $20^{\prime \prime}$ |
|  | GLCS | 7.44\# | $20^{\prime}$ | $48^{\prime \prime}$ | $24^{\prime \prime}$ | $48^{\prime \prime}$ |
|  | AL | 4.87\# | $20^{\prime}$ | $30^{\prime \prime}$ | $48^{\prime \prime}$ | $48^{\prime \prime}$ |
|  | GLCSL | 10.71\# | 25 | $48^{\prime \prime}$ | $24^{\prime \prime}$ | $48^{\prime \prime}$ |
|  | Glcalx | 1101\# | $30^{\prime}$ | $48^{\prime \prime}$ | $24^{\prime \prime}$ | $48^{\prime \prime}$ |
| 1000\# | GLC | 6.22\# | 6 | $8{ }^{\prime \prime}$ | $24^{\prime \prime}$ | $20^{\prime \prime}$ |
|  | GLCS | 12.25\# | 20 | 48 | 24 | 48 |
|  | AL | 8.36\# | $20^{\prime}$ | $30^{\prime \prime}$ | $48^{\prime \prime}$ | $48^{\prime \prime}$ |
|  | GLCSL | 14.08\# | 25 | $48^{\prime \prime}$ | $24^{\prime \prime}$ | $48^{\prime \prime}$ |
|  | GLCSLX | 17.47\# | $30^{\prime}$ | $48^{\prime \prime}$ | $24^{\prime \prime}$ | $48^{\prime \prime}$ |
| 2000\# | GLC | 9.12\# | 6 | $8{ }^{\prime \prime}$ | $24^{\prime \prime}$ | $24^{\prime \prime}$ |
|  | GLCS | 16.89\# | $20^{\prime}$ | $48^{\prime \prime}$ | $24^{\prime \prime}$ | $48^{\prime \prime}$ |
|  | AL | 10.01\# | $20^{\prime}$ | $30^{\prime \prime}$ | $48^{\prime \prime}$ | $48^{\prime \prime}$ |
|  | GLCSL | 19.36\# | 25 | $48^{\prime \prime}$ | $24^{\prime \prime}$ | $48^{\prime \prime}$ |
|  | GLCSLX | 20.13\# | $30^{\prime}$ | $48^{\prime \prime}$ | $24^{\prime \prime}$ | $48^{\prime \prime}$ |
| 4000\# | GLC | 9.12\# | 6 | $8{ }^{\prime \prime}$ | $24^{\prime \prime}$ | $24^{\prime \prime}$ |
|  | GLCS | 20.68\# | $20^{\prime}$ | $48^{\prime \prime}$ | $24^{\prime \prime}$ | $48^{\prime \prime}$ |
|  | GLCSL | 26.21\# | 25 | $48^{\prime \prime}$ | $24^{\prime \prime}$ | $48^{\prime \prime}$ |
|  | GLCSLX | 28.22\# | $30^{\prime}$ | $48^{\prime \prime}$ | $24^{\prime \prime}$ | $48^{\prime \prime}$ |

$R 1=\left(1.4^{*} P\right)+\left(W^{*} L 1\right)+\frac{\left(W^{*} L 4\right.}{2}$
$R 2=\left[(1.15\right.$ * $\left.P)+\frac{\left(w^{*} L 4\right)}{2}\right] * 0.10$
$R 3=1.15$ * $P$ * 0.20
Track supplied by Mortuary Lift Company highlighted in Red

